STATE OF VERMONT PUBLIC SERVICE BOARD

Petition of Vermont Gas Systems, Inc.,) requesting a Certificate of Public Good pursuant) to 30 V.S.A. § 248, authorizing the construction) of the "Addison Natural Gas Project") consisting of approximately 43 miles of new) natural gas transmission pipeline in Chittenden) and Addison Counties, approximately 5 miles of) new distribution mainlines in Addison County,) together with three new gate stations in) Williston, New Haven, and Middlebury,) Vermont)

Docket No. 7970

2-28-13 SUPPLEMENTAL PREFILED TESTIMONY OF JOHN HEINTZ ON BEHALF OF VERMONT GAS SYSTEMS, INC.

February 28, 2013

Mr. Heintz is the Project Manager for the Addison Natural Gas Project. His supplemental testimony describes the revised Project design, construction and schedule and provides an estimate of the Project costs. Mr. Heintz also describes construction-related impacts with respect to noise, water supply, waste disposal and transportation.

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2/28/13 EXHIBITS

Exhibit Petitioner Supp. JH-2 (2/28/13)	ANGP Project Map
Exhibit Petitioner Supp. JH-3 (2/28/13)	Transmission Mainline Engineering Plans
Exhibit Petitioner Supp. JH-4 (2/28/13)	Site Plan for Colchester Tie-In
Exhibit Petitioner Supp. JH-5 (2/28/13)	Distribution Mainlines Engineering Plans
Exhibit Petitioner Supp. JH-7 (2/28/13)	Site Plan for the Williston Road, Williston Gate Station
Exhibit Petitioner Supp. JH-8 (2/28/13)	Site Plan for the Plank Road, New Haven Gate Station
Exhibit Petitioner Supp. JH-9 (2/28/13)	Site Plan for the Exchange Street, Middlebury Gate Station
Exhibit Petitioner Supp. JH-10 (2/28/13)	Typical Sectionalizing Valve Site
Exhibit Petitioner Supp. JH-11 (2/28/13)	Project Cost Estimate

Exhibit Petitioner Supp. JH-14 (2/28/13)	Impact Minimization/Avoidance, Pipeline Reroutes and Alignment Shifts
Exhibit Petitioner Supp. JH-15 (2/28/13)	Impact Minimization/Avoidance, Through Horizontal Directional Drill (HDD)
Exhibit Petitioner Supp. JH-16 (2/28/13)	Impact Minimization/Avoidance, Through Right-of-Way Narrowing

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1 **1.** Introduction

- 2 Q1. Please state your name, occupation, and business address.
- 3 A1. My name is John Heintz. I am the President of International Engineering and
- 4 Development Corporation and have been retained by Clough Harbour & Associates
- 5 ("CHA") to serve as Project Manager of the Vermont Gas Systems, Inc. ("Vermont Gas"
- 6 or "VGS" or the "Company") Addison Natural Gas Project ("Project" or "ANGP"). My
- 7 business address is 2812 Shipping Ave, Miami, FL 33133.

- 9 Q2. What is the purpose of your testimony?
- 10 A2. My testimony and exhibits provide a detailed description of the revised Project layout
- 11 and engineering design, including the refinements and modifications undertaken since the
- 12 December 20, 2012 initial filing in this proceeding, referenced herein as either the

1		"December 20 Proposal" or the "Initial Proposal". The result of these revisions is
2		referred to here and in other witnesses' testimony as the "2/28/13 Alignment."
3		
4		My testimony also describes the equipment specifications and the pipeline construction
5		process that will be involved in building the Project. I also provide an updated Project
6		cost estimate. Finally, for ease of reference, I am also restating and including those
7		portions of my original testimony that are not changed.
8		
9		2. <u>Revised Project Description</u>
10	Q3.	Please describe the revised Project.
11	A3.	The Project includes the following principal components:
12		(1) Approximately 41.2 miles of new 12-inch transmission pipeline, extending
13		from a new tie-in to be located at Vermont Gas's existing 10-inch mainline north
14		of Severance Road in Colchester ("Colchester Tie-In"), Vermont, to the
15		intersection of U.S. Route 7 and Exchange Street in Middlebury, Vermont (the
16		"Transmission Mainline"). The initial Project contained 43 miles of 12-inch
17		transmission.
18		(2) Approximately 5.1 miles of new six-inch distribution mainlines ("Distribution
19		Mainlines") that will extend distribution service to Vergennes (3.73 miles) and
20		Middlebury (1.35 mile). The initial Project contained 4.8 miles of six-inch
21		distribution mainlines; and

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1		(3) Three new pressure regulation stations ("Stations" or "Gate Stations"), one
2		located near Route 2 in Williston to reinforce the existing distribution system, one
3		off Plank Road in New Haven, and the third north of the intersection of U.S.
4		Route 7 and Exchange Street in Middlebury. The number of gate stations is
5		unchanged, however this 2/28/13 Alignment reflects modified locations and
6		configurations in response to community feedback as discussed below.
7		
8		The Transmission Mainline is approximately 41.2 miles in length from the point of
9		interconnection in Colchester to the terminus at the new Route 7 Gate Station in
10		Middlebury. As with the initial proposal, the line will pass through the towns of
11		Colchester, Essex, Williston, St. George, Hinesburg, Monkton, New Haven and
12		Middlebury.
13		
14		The Distribution Mainline to Vergennes will extend from a new Plank Road Gate Station
15		in New Haven, running along Plank Road 3.7 miles through the towns of New Haven,
16		Ferrisburgh and Waltham, to the intersection of Route 7 in Waltham, just east of
17		Vergennes. The Middlebury Distribution Mainline will extend from the new Route 7
18		Gate Station in Middlebury to the Middlebury industrial park on Exchange Street.
19		
20		2.1 <u>Transmission Mainline from Colchester to Middlebury</u>
21	Q4.	Please describe the Transmission Mainline and the proposed alignment changes.

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1	A4.	A one page map with the revised 2/28/13 Alignment is included as Exhibit Petitioner
2		Supp. JH-2 (2/28/13). Detailed engineering plan sheets of the 2/28/13 Alignment
3		Transmission Mainline with design details are included as Exhibit Petitioner Supp. JH-3
4		(2/28/13). There have been a number of revisions to VGS' proposed transmission
5		pipeline alignment from the Petition submitted to the Board on December 20, 2012 (the
6		"Initial Proposal") to the 2/28/13 Alignment. These revisions have been developed in
7		response to stakeholder comments.
8		
9		In addition to the summary of alignment changes from the Initial Proposal to the $2/28/13$
10		Alignment, the following adjustments occurred throughout the alignment:
11		• An approximate one to five foot shift of the pipeline alignment where it parallels
12		the VELCO corridor due to improved Right-Of-Way information;
13		• The three Stations have been moved;
14		• and the Mainline Valve locations have shifted along the proposed pipeline relative
15		to the new Transmission pipeline length and Station locations.
16		
17		Below is a list of specific locations with alignment changes, with reference to specific
18		Exhibit Petitioner Supplement JH-3 (2/28/13) plan sheets. It should be noted that with
19		the exception of the gate stations described above and those locations where the pipeline
20		has been moved from road rights-of-way to adjacent to or within the VELCO corridor in
21		Hinesburg, Monkton and New Haven, most of the adjustments listed below are minor
22		alignment adjustments generally within the same vicinity:

1		
2	-	ANGP-T-C-001 Specification of the dewatering area west of Colchester Tie-In
3	-	<u>ANGP-T-C-005</u> - Change in additional temporary work space (ATWS) areas near
4		MP 2.2 (Route 2A)
5	-	ANGP-T-C-018 - Transmission Mainline alignment change at MP 8.6 to avoid
6		VELCO infrastructure (500 feet)
7	-	ANGP-T-C-021 - Transmission Mainline alignment change at Allen
8		Brook/Route 2 crossing (MP 10.3) and addition of an ATWS south of Route 2
9		(1,100 feet) for Horizontal Directional Drilling (HDD) purposes
10	-	ANGP-T-C-021&022 - Williston gate station (MP-10.45) moved to the east 300
11		feet along Transmission Mainline
12	-	ANGP-T-C-023B - Alignment change at I-89 crossing to Hurricane Lane (MP
13		11.4) and concurrent pullback area shift (1,400 feet)
14	-	ANGP-T-C-027 & 028 – Transmission Mainline alignment shift further east of
15		VELCO (K-23) ROW (MP 13.5) north of Williston Switching Station (600 feet)
16	-	ANGP-T-C-028 – Transmission Mainline alignment shift from west to east side
17		of VELCO K-43 ROW from MP 13.84 to MP 14.25 (2,200 feet)
18	-	ANGP-T-C-031 & 032 – Transmission Mainline alignment shift into VELCO K-
19		43 ROW at MP 15.6 (1,500 feet)
20	-	ANGP-T-C-034 & 035 – Transmission Mainline re-alignment along Route 116 to
21		Route 2A Crossing (MP 16.9) (1,700 feet)

1	-	ANGP-T-C-036 – Transmission Mainline alignment shift toward VELCO K-43
2		ROW (MP 17.35) (700 feet)
3	-	ANGP-T-C-041 - 049 – Transmission Mainlinealignment change from along
4		Charlotte/Baldwin Rd to VELCO K-43 ROW and parallel VELCO line (MP 19.8
5		to 24) (22,200 feet)
6	-	<u>ANGP-T-C-050 - 052</u> – Transmission Mainline alignment change from VELCO
7		K-43 ROW to (MP 24 to MP 24.9), crossing Rotax Rd. (4,800 feet)
8	-	<u>ANGP-T-C-053 – 061A</u> – Transmission Mainline alignment change from along
9		Monkton Rd to continuing to follow VELCO K-43 ROW, with HDD under
10		Monkton Swamp and with access from Split Rock Rd, to Old Stage Rd (MP
11		25.75 to MP 28.9) (16,600 feet)
12	-	<u>ANGP-T-C-063 - 068</u> – Transmission Mainline alignment change from along Old
13		Stage Rd/Parks-Hurlburt Rd/North St (MP 29.65) to west side of VELCO K-43
14		ROW to Plank Rd (MP 32.4) (14,500 feet)
15	-	ANGP-T-C-068 - Plank Rd gate station moved from east of North St/Plank Rd
16		intersection to west side of VELCO K-43 ROW at MP 32.5
17	-	ANGP-T-C-072 – Transmission Mainline alignment shift from west side of
18		VELCO K-64 ROW to cross Route 17 (Main St) and parallel New Haven
19		Substation access (MP 34.6 – MP-35.1)) (2,640 feet)
20	-	<u>ANGP-T-C-074</u> – Transmission Mainline alignment change under VELCO K-64
21		ROW and crossing Town Hill Rd (MP 35.6) (1,050 feet)

1	- <u>ANGP-T-C-083A - 085</u> – Transmission Mainline alignment change from east side
2	of Route 7 at River Rd intersection to west side with ATWS on north west corner
3	of Belden Falls Rd/Route 7 intersection (MP 40.3 to 41.2 end of ANGP
4	transmission mainline) (4,800 feet)
5	- <u>ANGP-T-C-085</u> - Middlebury gate station moved from south of Exchange
6	St/Route 7 intersection, ~0.5 miles north
7	- <u>ANGP-T-C-085</u> - Change from Transmission to Distribution Mainline from end
8	of ANGP at Middlebury Gate Station (MP 41.2) along west side of Route 7 to
9	Exchange St/Route 7 intersection (2,400 feet)
10	
11	At the point of interconnection with the existing VGS transmission system in Colchester,
12	the Colchester Tie-In will be reconfigured with an approximately 35-foot by 85-foot
13	fenced-in yard to enclose the valve and an area for utilizing a pipeline in-line cleaning or
14	inspection tool or "PIG" launcher. This is a slightly larger footprint to better
15	accommodate the necessary infrastructure. A PIG is a tool used in the industry to clean
16	the pipe or to inspect the integrity of the pipeline walls for things such as defects or
17	corrosion. It moves down the pipeline by the force of the natural gas pressure in the
18	pipeline. The fence will be a galvanized chain-link metal fence approximately 6 feet in
19	height with three strands of barbed wire extending another foot. The fenced area will
20	have a pervious crushed stone surface underlain by a geogrid to infiltrate rainwater and
21	snowmelt. An access road, approximately 1,000 feet long, consisting of 470 feet of
22	existing paved driveway and 530 feet of new stabilized pervious surface driveway will

- extend from Severance Road to the Colchester Tie-In. Exhibit Petitioner Supp. JH-4
 (2/28/13) is a site plan for the Colchester Tie-In.
- 3

4	To optimize the alignment of the Transmission Mainline corridor, Vermont Gas has
5	attempted to co-locate the pipeline with, or adjacent to, other utility and road
6	infrastructure where possible, in order to minimize impacts. The northern segment of the
7	Transmission Mainline, from Colchester to Williston near Interstate 89, will generally be
8	located within the ROW of VT 289 (also referred to as the Circumferential Highway,
9	"CCCH" or "CIRC"). This segment of the Project corridor is approximately 11 miles
10	from the Colchester Tie-In, and extends though portions of the towns of Colchester,
11	Essex and Williston, to a point east of Interstate 89 in Williston, near the intersection of
12	Interstate 89 and U.S. Route 2.
13	
14	Near the intersections of Interstate 89 and Route 2 in Williston, the Transmission
15	Mainline will leave the CIRC corridor. The Transmission Mainline continues south,

- 16 within or adjacent to an existing Vermont Electric Power Company, Inc. ("VELCO")
- 17 electric transmission line corridor that extends between Williston and Middlebury,
- 18 Vermont. This segment of the Transmission Mainline extends about 30 miles and crosses
 19 through portions of the towns of Williston, St. George, Hinesburg, Monkton, New Haven
- 20 and Middlebury. The details for this approximately 30-mile southern segment of the
- 21 Transmission Mainline are shown in the Transmission Mainline Alignment Sheets,
- 22 Exhibit Petitioner Supp. JH-3 (2/28/13).

2	A more detailed summary of the Transmission Mainline 2/28/13 Alignment is as follows:
3	• The proposed 12-inch transmission pipeline connects to an existing VGS 10-inch
4	transmission pipeline in Colchester, VT. The pipeline exits this location (Colchester
5	Tie-In Site) and runs west for approximately 0.1-miles within the existing VGS ROW
6	to the northerly ROW edge of the un-built CCCH. The pipeline runs parallel to the
7	ROW edge and within the CCCH ROW for approximately 2.1-miles crossing Mill
8	Pond Road (MP-0.49), passing under Indian Brook (MP 0.99), crossing VELCO's K-
9	22 transmission line (MP-1.3), passing under Indian Brook for a second time (MP-
10	1.5), and crossing Route 2A and New England Central Railroad (MP-2.1); avoiding
11	along the way, present and future constructability issues. This segment of the $2/28/13$
12	Alignment is essentially unchanged from the December 20, 2012 proposal.
13	

14 The alignment then drops off the un-built CCCH ROW and runs along Route 289, • 15 approximately 40-ft off the edge of pavement for 0.9-miles until the pipeline crosses VELCO at MP-3.0. After crossing VELCO, the pipeline works its way back to the 16 17 edge of Route 289 ROW, where again it parallels the ROW edge for a distance of 3miles; crossing Indian Brook a third time (MP-3.6), crossing Route 15 (MP-4.1), 18 19 Essex Way (MP-4.55), Alder Brook 9MP-5.05), and Alder Brook again (MP-6.25). 20 The only substantive change in this segment is a location change for a temporary 21 work space.

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1 Over the next 0.65-miles the alignment makes a cross country approach for a ٠ 2 horizontal directional drill crossing under the Winooski River (MP-6.85) and Route 3 117 (MP-6.76), coming up on the south side of the river adjacent to Vermont Central 4 Railroad (MP-7.0). The pipeline crosses under Vermont Central Railroad, and runs 5 alongside the same for 0.1-miles and crosses another section of the un-built CCCH. crosses the Burlington Transfer Station site and Chittenden Solid Waste and picks up 6 7 Redmond Road (MP-7.56), the location of VGS' first Mainline Valve. This segment 8 is essentially unchanged from the Initial Proposal. 9 10 The alignment runs south along the eastern edge of the Redmond Road ROW for 11 1.44-miles, then along the northern edge of Mountain View Road ROW for 0.1-miles 12 before crossing Mountain View Road and re-entering the CCCH highway, where the 13 Transmission Mainline follows the westerly edge of the un-built CCCH highway for 14 1-mile, makes an approach for and crosses Allen Brook (MP-10.3), Route 2 (Williston Rd), avoiding conflicts with sensitive environmental areas, and the 15 16 possible future extension of the CCCH. On the south side of Williston Road, VGS proposes constructing the first of three Gate Stations (MP-10.45). The change of note 17 18 in this segment is the shift of the Williston Station approximately 300 feet to the east. 19 20 Upon leaving the Williston Station the pipeline re-enters the un-built CCCH • 21 ROW at its western edge and continues southerly to Interstate 89 and then west along 22 I89 to MP-11.3 the location of the I89 crossing, thus avoiding potential conflicts with

1	the existing VELCO Sub Station infrastructure on the south side of I89 and the
2	stakeholders along Hurricane Lane. The distance between the Gate Station and the
3	I89 crossing location is approximately 0.85-miles. Any changes from the December
4	20, 2012 proposal in this area are minor.
5	
6	• After crossing I89, the pipeline runs along the southerly edge of Hurricane Lane,
7	for 0.2-miles, crosses to the west side of the VELCO ROW, avoiding existing utility
8	infrastructure before generally running along and parallel to VELCO to the St.
9	George/Williston town line (MP-14.7). In this section, the pipeline crosses VELCO
10	at MP-12.35, St. George Road at MP-12.42, VELCO at MP-12.52, VELCO at MP-
11	13, across Sucker Brook at MP-13.8, then south to VGS' second mainline valve
12	location north of Lincoln Rd (MP-14.3), across Lincoln Rd (MP-14.31) and on to the
13	St George/Williston town line. Any changes from the December 20, 2012 proposal in
14	this area are minor.
15	
16	• After crossing the St. George/Williston town line the transmission pipeline leaves
17	the VELCO ROW to avoid stakeholder and constructability issues. This segment is
18	essentially unchanged from the Initial Proposal.
19	
20	• At MP-15.2 the alignment crosses the VELCO ROW to its western side, the
21	alignment continues southerly generally parallel to the VELCO ROW western side
22	(MP 15.3 to 16.2). This segment is essentially unchanged from the Initial Proposal

- except for approximately 1,500 feet of pipeline that has been shifted into the VELCO
 ROW.
- The alignment then crosses the VELCO ROW (MP-16.2) and continues southerly
 0.8 miles (MP 16.2 to 17.0) until crossing Route 2A (MP-16.8), Route 116 (MP16.92), and VELCO again at MP-17.0. Any changes from the December 20, 2012
 proposal in this area are minor.
- 7
- 8 The alignment then continues southerly just west of VELCO to address 9 landowner concerns and aligns with and parallels the VELCO ROW just inside the 10 Hinesburg town line (MP-17.4 to MP-18.1), then moves west to avoid a tributary to 11 the Laplatte River, crosses Shelburne Falls Road (MP-18.94) and joins back up with 12 the western side of the VELCO ROW (MP-19.2), crosses under the Laplatte River 13 MP-19.5 to VGS third mainline valve located at MP-19.81, just north of Charlotte 14 Road in Hinesburg. Any changes from the December 20, 2012 proposal in this area are minor. 15
- 16

The pipeline crosses Charlotte Road, continues southerly parallel to and 270 Ft.
offset from the western VELCO ROW avoiding a meandering stream and wetlands
for 0.9-miles (MP 19.9 to 20.8) where it re-enters the VELCO ROW. The 2/28/13
Proposal has been relocated off of Baldwin Road to a location that parallels the
VELCO ROW.

1	• The pipeline continues 10 Ft. inside the western edge of VELCO crossing
2	Baldwin Road (MP-21.1) and Drinkwater Road (MP-22.34) and Lewis Creek (MP-
3	22.86) for 4.1-miles (MP 19.9 to 24.0). The 2/28/13 Proposal has been relocated off
4	of Baldwin Road to a location within the VELCO ROW.
5	
6	• The alignment leaves VELCO in the vicinity of Rotax Road in Monkton (i.e. the
7	"Rotax Road Reroute") and continues southerly 0.9 miles (MP 24.0 to 24.9). The
8	Initial Proposal was along public road ROW. The Rotax Road Reroute was selected
9	due to constructability and landowner concerns.
10	
11	• The alignment meets the VELCO ROW and continues southerly 0.9 miles (MP
12	24.9 to 25.8) parallel to and along the westerly side. The $2/28/13$ Proposal has been
13	relocated off of public road ROWs to a location adjacent to the VELCO ROW.
14	
15	• The alignment enters and continues 10-ft inside the VELCO ROW for 1.5 miles
16	(MP 25.8 to 27.3), crossing Stillson Road (MP-26.1), and Hollow Road (MP-25.4).
17	VGS' fourth mainline valve is proposed just south of Hollow Road in Monkton (MP-
18	26.48). The 2/28/13 Proposal has been relocated off of the public road ROW to a
19	location within the VELCO ROW.
20	
21	• The pipeline then continues west under Monkton Swamp using HDD, MP-27.3 –
22	MP-27.65 and then back to and 10-ft inside the VELCO ROW at MP-28. The

- 2/28/13 Proposal has been relocated off of the public road ROW to a location within or parallel to the VELCO ROW.
- 3

2

The pipeline continues inside VELCO's ROW until Old Stage Road, where it 4 5 then runs within the Old Stage Road ROW (MP-28.9 to MP-29.63) to avoid a meandering stream and wetland. At MP 29.63, the Transmission Mainline crosses 6 7 from Old Stage Road through approximately 330 feet of open field to the western 8 edge of the VELCO ROW and continues southerly 10 ft within and parallel to 9 VELCO until MP-31.6, crossing Parks -Hurlburt Road (MP-30.1) and the Monkton, 10 New Haven town line (MP-31.1). The 2/28/13 Proposal has been primarily relocated 11 off of the public road ROW to a location within the VELCO ROW.

12

13 The proposed alignment then continues outside and parallel to the VELCO ROW 14 3.2 miles (MP 31.6 to 34.8) crossing Little Otter Creek (MP-32.3), Plank Road (MP-15 32.5), Quarry Road (MP-33.5), Route 17 (MP-34.9), and into the VELCO New 16 Haven Substation property (MP-34.9 - MP-35.51). VGS' proposed fifth mainline valve is located at MP-32.39. The alignment then continues 0.6 miles (MP 35.1 to 17 18 35.7) briefly leaving VELCO to avoid structures and crossing Town Hill Road (MP-19 35.64) and VELCO to the eastern edge of VELCO. The most significant adjustment 20 from the Initial Proposal is the shift of the New Haven Station location approximately 21 a quarter mile west.

1		• The proposed alignment continues outside and parallel to the eastern edge of
2		VELCO to MP-36.4 wherein the pipeline crosses VELCO and runs parallel to and
3		outside the VELCO ROW to River Road (MP-39.54), crossing Hunt Road (MP-38.1)
4		where Mainline Valve 6 will be installed and then crossing the New Haven River
5		(MP-39.35). Any changes from the December 20, 2012 proposal in this area are
6		minor.
7		
8		• The pipeline continues westerly inside and outside the northerly ROW of River
9		Road crossing to the westerly edge of Route 7, where it continues south 10 ft. outside
10		and parallel to the road ROW terminating at the Proposed Middlebury Station (MP
11		41.23). The $2/28/13$ Proposal changes the pipeline and the Station from the east side
12		of Route 7 to the west.
13		
14	Q5.	Please describe the design specifications for the Transmission Mainline.
15	A5.	The engineering design was guided by applicable federal and state standards including
16		the following, which have not changed from the Initial Proposal:
17		• U.S. Department of Transportation, Office of Pipeline Safety, Code of Federal
18		Regulations Title 49, Part 192 – Transportation of Natural and Other Gas by
19		Pipeline: Minimum Safety Standards ("Code");
20		• American Society of Mechanical Engineers ("ASME") B31.8 – Gas Transmission
21		and Distribution Piping Systems;

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1	• Vermont Public Service Board General Order #43, Rules and Regulations
2	Prescribing Standards for Gas Utilities;
3	• American Petroleum Institute ("API") 5L, Specification for Line Pipe, 2009;
4	• API Specification 6D, Specification for Pipeline Valves, 2008;
5	• American Society for Testing and Materials ("ASTM") A53/A53M-07, Standard
6	Specification for Pipe, Steel, Black and Hot Dipped, Zinc Coated, Welded and
7	Seamless;
8	• ASTM D2513-99, Standard Specification for Thermoplastic Gas Pressure Pipe,
9	Tubing and Fittings;
10	• MSS-Standard Practice SP-44-2006 Standard Practice, Steel Pipeline Flanges;
11	and
12	• Vermont Public Service Board Rule 6.100.
13	
14	The Transmission Mainline will be designed and constructed to a Maximum Allowable
15	Operating Pressure ("MAOP") of 1,440 pounds per square inch ("psi"). The pipeline will
16	be constructed of carbon-steel pipe (12.75-inch outside diameter), with a wall thickness
17	of 0.283 inches in Class II (rural) ¹ areas and 0.312 inches for the remainder of the route.
18	The pipe material will have a specified minimum yield strength of 65,000 psi. For Class
19	III areas, a design factor of 0.5 was used in the design pressure calculation, and for Class
20	I and II areas a design factor of 0.6 was used, both of which are more stringent than

¹Class location is the term used in the Code (49 C.F.R. Part 192) to classify the population density in the vicinity of the pipeline. The design of a pipeline may vary depending on the class location of the pipeline. Please refer to Mr. Teixeira's testimony for further explanation of this class location system.

1		required by the Code. This will allow the design pressure to stay the same even if there is
2		a future change in the class location of the pipeline. The pipe will be manufactured in
3		accordance with the API 5L, Specification for Line Pipe.
4		
5		The pipe will have an external, corrosion-control coating; the coating will vary dependent
6		upon soil conditions but in general it will consist of 15 mils thickness of fusion bond
7		epoxy or Pritec. Segments of pipe to be installed by horizontal directional drill ("HDD")
8		will have an additional 40 mils thickness of abrasion resistant coating over the external
9		control coating. Cathodic protection will be provided by an impressed current rectifier
10		system. The pipe will be hydrostatically-tested at a pressure of 1.5 times MAOP, at
11		2,160 psi for a minimum of eight hours before being placed in service. The test will
12		assure there are no leaks and validate the MAOP of 1,440 psi. I discuss this testing
13		below.
14		
15		The pipeline will be entirely welded in accordance with API recommended practice
16		standard 1104 – Welding of Pipelines and Related Facilities. All welds will be
17		nondestructively tested in accordance with API 1104 by x-ray techniques. The test
18		records will be kept for the life of the facility.
19		
20	Q6.	What is the width of the Transmission Mainline corridor?
21	A6.	Generally, the Transmission Mainline corridor will occupy a 50-foot wide permanent
22		ROW, together with a 25-five foot temporary easement area that will be used to complete

1		construction. This too is unchanged from the Initial Proposal. Vanasse Hangen Brustlin,
2		Inc. ("VHB") has studied up to a 300-foot wide area for purposes of conducting its
3		environmental resource impact analysis for this Section 248 application.
4		
5		In areas where construction will parallel a public road ROW, VGS will utilize a 20-foot
6		ROW on private land adjacent to the road ROW where possible. If obtaining a ROW on
7		private land is not possible, the pipeline will be located in the public ROW and the
8		construction crews will utilize the road as work space. The entire ROW on the side of the
9		road where the pipeline will be located will be cleared of vegetation in order to allow for
10		construction. After completion of construction, the disturbed ROW area will be graded
11		back to its previous contours and restored consistent with the Erosion Prevention and
12		Sediment Control Plan (provided as an attachment to Exhibit Petitioner Supp. JAN-9
13		2/28/13).
14		
15	Q7.	Earlier you mentioned a number of reroutes and revisions that occurred to accommodate
16		sensitive environmental and cultural resources along the route first identified in the
17		Preliminary Alignment for the Transmission Mainline. Please summarize those
18		revisions.
19	A7.	Designing the Project is a complex, interdisciplinary and iterative process that has taken
20		months to develop. Once the CIRC and VELCO corridors were identified as the
21		Preliminary Alignment for the Transmission Mainline (the process for which is more
22		fully discussed in Mr. Howe's prefiled testimony), VGS hired CHA and environmental,

1	archaeological and aesthetic consultants to undertake detailed assessments of the
2	Preliminary Alignment. Based upon that input, we continued to refine the Project design
3	in dozens of locations to avoid or minimize impacts. With this 2/28/13 Proposal we have
4	continued to minimize impacts as well as address community concerns. We have
5	modified over 21 miles or about 51% of the Preliminary Alignment in order to avoid or
6	mitigate these sensitive resource areas, as follows:
7	• 16 miles (pipeline reroutes and alignment shifts)
8	• 7.6 miles (narrowing of ROW)
9	• 3.6 miles (HDD)
10	Please refer to Exhibits Petitioner Supp. JH-14 (2/28/13) (Impact
11	Minimization/Avoidance, Pipeline Reroutes and Alignment Shifts), JH-15 (2/28/13)
12	(Impact Minimization/Avoidance, Through Horizontal Directional Drill) and JH-16
13	(2/28/13) (Impact Minimization/Avoidance, Through Right-of-Way Narrowing).
14	
15	One significant re-route from the Preliminary Alignment is located on the southern side
16	of the Winooski River in the area parallel to Redmond Road in Williston. There, the
17	2/28/13 Alignment, like the Initial Proposal, will extend west of the CIRC to connect to
18	Redmond Road near the Chittenden Solid Waste Facilities, and continue south and
19	southeast along Redmond Road at a point where Mountain View Road in Williston meets
20	up with the CIRC corridor. This re-route, the so-called "Redmond Road Re-Route" is
21	approximately 1.9 miles in length. This change to the Preliminary Alignment along the
22	CIRC was undertaken by VGS following input from regulators and stakeholders in order

1		to avoid and minimize potential impacts to forested wetlands and wetland habitat, as		
2		discussed in more detail in the testimony and exhibits of Jeffrey Nelson of VHB. These		
3		areas are depicted on the Transmission Mainline Alignment Plans, Exhibit Petitioner		
4		Supp. JH-3 (2/28/13). Mr. Nelson also addresses this re-route in his testimony and		
5		exhibits.		
6				
7		The approximately 7.4 miles of the pipeline ROW that was narrowed from 75 feet to 50		
8		feet, results in an approximate 7.4-acre reduction in wetland impacts. The reduction of		
9		ROW width will result in additional costs to the Project which are currently estimated at		
10		approximately \$1.2 million. These additional costs are also included in the Project Cost		
11		Estimate, Exhibit Petitioner Supp. JH-11 (2/28/13).		
12				
13	Q8.	What other measures will be taken to minimize impacts?		
14	A8.	Because of the nature of a long, linear pipeline expansion project such as this, complete		
15		avoidance of all environmental and cultural resource areas is not possible, but a number		
16		of precautions will be taken to minimize impacts. In wetlands and agricultural areas,		
17		where trenches are used, soil horizons will be removed in order and stockpiled so that		
18		horizons can be restored as closely as possible to pre-construction conditions. In some		
19		cases, we will employ coffer dams for stream crossings and we will use matting for all		
20		work in wetland areas. Silt fences and other erosion control techniques will be used, as		
21		well as matting, construction limit barriers, etc. Mr. Nelson's testimony describes the		

1	techniques that will be employed to minimize environmental impacts to sensitive areas
2	during Project construction.
3	
4	As I have also noted, where appropriate, we will horizontally directional drill under
5	certain streams, rivers, wetlands, and other resources. These areas include:
6	Indian Brook, MP 0.9;
7	Indian Brook, MP 1.3;
8	Indian Brook, MP 3.6;
9	Winooski River, MP 6.7;
10	Allen Brook, MP 10.3;
11	LaPlatte River, MP 19.6;
12	Resources near Drinkwater Road, MP 22.1;
13	Lewis Creek, MP 22.6;
14	Monkton Swamp, MP 27.2:
15	VT AD-1560&1561-Locus 1 and 2 (Arch Sites), South of Monkton Road, MP
16	28.2:
17	VT AD-1562 (Arch Site), South of Monkton Road, MP 28.6:
18	VT AD 446 (Arch site), North of Quarry Road, MP 33.2;
19	VT AD 793(Arch site), Locus 2 and 3, MP 33.7;
20	VT AD 806 (Arch Site) South of Town Hill Road, MP 35.8;
21	VT AD 808 (Arch Site), MP 36;
22	New Haven River, MP 39.35.

1		
2		The use of HDD in these areas has eliminated over 6.7 acres of wetland impact, nearly
3		60,000 square feet of stream impact, impact to four rare, threatened and endangered
4		species habitat and nine archaeological sites. The additional cost associated with the
5		installation of HDDs in these areas is approximately \$5.4 million and is reflected in the
6		Project Cost Estimate, see Exhibit Petitioner Supp. JH-11 (2/28/13).
7		
8		These areas are identified in Exhibit Petitioner Supp. JH-15 (2/28/13).
9		
10		2.2 <u>Distribution Mainlines to Vergennes and Middlebury</u>
11	Q9.	Please describe the Distribution Mainlines.
12	A9.	There are two Distribution Mainlines. The site plans are included as Exhibit Petitioner
13		Supp. JH-5 (2/28/13). The first is a 3.7-mile segment of 6-inch polyethylene ("PE") pipe
14		that will begin at the new Plank Road Gate Station in New Haven, that runs through the
15		Towns of New Haven, Ferrisburgh, and Waltham, to the intersection of Route 7 in
16		Waltham, just east of Vergennes (the "Vergennes Distribution Mainline"). Network
17		construction will begin at this point extending into the City of Vergennes. As a result of
18		the change in the location of Plank Road Station, the Vergennes Distribution Mainline is
19		slightly shorter than the Initial Proposal.
20		
21		The second Distribution Mainline is also 6-inch PE pipe which will run approximately
22		1.35 miles along Route 7 and Exchange Street in Middlebury, between the new

1		Middlebury Station and into the Middlebury industrial park. As a result of the change in		
2		the location of Middlebury Station, the Middlebury Distribution Mainline is slightly		
3		longer than the Initial Proposal.		
4				
5		Both Distribution Mainlines will be located within the public ROWs of Plank Road and		
6		Route 7/Exchange Street. The Project plans for the Distribution Mainlines are included		
7		as Exhibit Petitioner Supp. JH-5 (2/28/13).		
8				
9		2.3 <u>Gate Stations and Valves</u>		
10	Q10.	Please describe each of the three Gate Stations.		
11	A10.	A gate station is a necessary component of a gas distribution system. The purpose of a		
12		gate station is to reduce the higher pressure in the transmission pipeline to the lower		
13		pressure used in the distribution network. A photograph of a VGS gate station was		
14		provided as Exhibit Petitioner JH-6.1.		
15				
16		The first Gate Station will be located near Route 2 in Williston to reinforce the existing		
17		distribution system. A site plan for the Williston Gate Station is included as Exhibit		
18		Petitioner Supp. JH-7 (2/28/13). It will include an approximately 55-foot by 85-foot		
19		fenced-in yard with a small parking area, an approximately 12-foot wide by 32-foot long		
20		precast concrete meter and regulator building, a-foot wide by 8-foot long SCADA ²		
21		building and an approximately 8-foot wide by 12-foot long concrete pad on which the		

²The acronym SCADA stands for "supervisory control and data acquisition."

1	pipeline heater will be mounted. Each enclosure building will be approximately 9 feet				
2	high from ground level to the roof peak. The enclosure buildings will house three major				
3	components of the Gate Station: (1) SCADA and telecommunica	components of the Gate Station: (1) SCADA and telecommunications equipment, (2) the			
4	pressure regulation equipment, and (3) the meter. A Dry-Line he	ater system will be			
5	installed outside on the concrete pad. A Dry-Line heater works b	by producing steam			
6	within a vacuum, and heating the gas passing through pipes with	within a vacuum, and heating the gas passing through pipes within the heater shell with			
7	low temperature steam.	low temperature steam.			
8					
9	Plantings will be installed to provide screening for the facility, as shown on the visual				
10	report provided by Michael Buscher, Exhibit Petitioner Supp. MJB-2.1 (2/28/13).				
11					
12	The design criteria for the Williston Gate Station are described as	follows:			
13	• Design maximum station inlet pressure (current):	605 psig			
14	• Design maximum station inlet pressure (future):	1440 psig			
15	• Design minimum station inlet pressure, at regulators:	250 psig			
16	• Design normal station inlet pressure, at regulators:	400 psig			
17	• Design maximum station outlet pressure:	100 psig			
18	• Design flow volume, summer:	350 Mcfh			
19	• Design flow volume, peak:	1,000 Mcfh			
20	• Design minimum flow volume:	50 Mcfh			
21	• Pipeline size into station:	6-inch			
22	• Station piping wall thickness: Sche	dule 80 or XH Seamless			

1	• Station piping grade:	Gr. B or X-42		
2	• Safety device:	Monitor and Relief		
3	• Relief set pressure at 110% of MOP:	110 psig		
4	• Inlet gas temperature:	32°F		
5	• Outlet gas temperature:	40°F		
6	• Heater:	CWT Dry-Line Heater		
7	• Filter:	PECO 30F		
8	• Meter:	6-inch Turbine		
9	• Odorizer:	N/A		
10	• Station outlet control methodology:	3-inch Grove 900TE		
11		Monitor/Regulator		
12				
13	The changes to the Williston Station from the Initial Prop	The changes to the Williston Station from the Initial Proposal are primarily related to a		
14	slight change in the equipment configuration. The footpri	int of the Williston Station is		
15	unchanged.			
16				
17	A second Gate Station will be located on Plank Road in New Haven to initially provide			
18	natural gas service to Vergennes. A site plan for the Plank Road Gate Station is included			
19	as Exhibit Petitioner Supp. JH-8 (2/28/13). It will include an approximately 85-foot by			
20	55-foot fenced-in yard with a small parking area, an approximately 12-foot wide by 32-			
21	foot long precast concrete meter and regulator building, an 8-foot wide by 8-foot long			

SCADA building and an approximately 8-foot wide by 12-foot long concrete pad on

1	which the pipeline heater will be located. Each enclosure b	ouilding will be approximately
2	9 feet high from ground level to the roof peak. The enclose	ure buildings will house three
3	major components of the Gate Station: (1) SCADA and tele	ecommunications equipment,
4	(2) the pressure regulation equipment, and (3) the meter. A	Dry-Line heater system will
5	be installed outside on the concrete pad. Plantings will be	installed to provide screening
6	for the facility, as shown on the visual report provided by M	Aichael Buscher, Exhibit
7	Petitioner Supp. MJB-2.1 (2/28/13).	
8		
9	The design criteria for the Plank Road Gate Station are as f	follows:
10	• Design maximum station inlet pressure (current):	605 psig
11	• Design maximum station inlet pressure (future):	1440 psig
12	• Design minimum station inlet pressure, at regulator	s:250 psig
13	• Design normal station inlet pressure, at regulators:	400 psig
14	• Design maximum station outlet pressure:	125 psig
15	• Design flow volume, summer:	250 Mcfh
16	• Design flow volume, peak:	400 Mcfh
17	• Design minimum flow volume:	25 Mcfh
18	• Pipeline size into station:	4-inch
19	• Station piping wall thickness:	Schedule 80 or XH Seamless
20	• Station piping grade:	Gr. B or X-42
21	• Safety device:	Monitor and Relief
22	• Relief set pressure at 110% of MOP:	137 psig

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1	• Inlet gas temperature:	32°F
2	• Outlet gas temperature:	40°F
3	• Heater:	CWT Dry-Line Heater
4	• Filter:	PECO
5	• Meter:	6-inch Turbine
6	• Odorizer:	N/A
7	• Station outlet control methodology: 2" Grove 900	TE Monitor/Regulator
8		
9	The changes to the Plank Road Station from the Initial Pro	posal are primarily related to a
10	slight increase in the footprint to accommodate changes in	the equipment configuration.
11		
12	The third Gate Station, the Middlebury Gate, will be locate	ed on the westside of Route 7
13	behind Paquette Enterprises Self Storage Facility in Middl	ebury. A site plan for the
14	Middlebury Gate Station is provided as Exhibit Petitioner	Supp. JH-9 (2/28/13). It will
15	include an approximately 55-foot by 85-foot fenced-in yar	d with a small parking area, an
16	approximately 12-foot wide by 32-foot long precast concre	ete meter and regulator
17	building, an 8-foot wide by 8-foot long SCADA building a	and an approximately 8-foot
18	wide by 12-foot long concrete pad on which the pipeline h	eater will be located. Each
19	enclosure building will be approximately 9 feet high from	ground level to the roof peak.
20	The enclosure buildings will house three major component	s of the Station: (1) SCADA
21	and telecommunications equipment, (2) the pressure regula	ation equipment, and (3) the
22	meter. A Dry-Line heater system will be installed outside	on the concrete pad. Plantings

1	will be installed to provide screening for the facility, as shown on the visual report
2	provided by Michael Buscher, Exhibit Petitioner Supp. MJB-2.1 (2/28/13).
3	
4	The design criteria for the Middlebury Gate Station are described as follows:
5	• Design maximum station inlet pressure (current): 605 psig
6	• Design maximum station inlet pressure (future): 1440 psig
7	• Design minimum station inlet pressure, at regulators:250 psig
8	• Design normal station inlet pressure, at regulators: 400 psig
9	• Design maximum station outlet pressure: 125 psig
10	• Design flow volume, summer: 350 Mcfh
11	• Design flow volume, peak: 500 Mcfh
12	• Design minimum flow volume: 75 Mcfh
13	• Pipeline size into station: 4-inch
14	• Station piping wall thickness: Schedule 80 or XH Seamless
15	• Station piping grade: Gr. B or X-42
16	• Safety device: Monitor and Relief
17	• Relief set pressure at 110% of MOP: 137 psig
18	• Inlet gas temperature: 32°F
19	• Outlet gas temperature: 40°F
20	Heater: CWT Dry-Line Heater
21	• Filter: PECO 30F
22	Meter: 6-inch Turbine

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1		• Odorizer:	N/A
2		• Station outlet control methodology:	3" Grove 900TE
3			Monitor/Regulator
4			
5		The Station configuration being proposed consists of	two separate regulator runs, with
6		one run serving as a full back up to the other. Each r	egulator run consists of two identical
7		regulators set up in what is termed a working and mo	nitor set. The Station will also
8		include a relief valve to provide a secondary device f	or overpressure protection. This
9		configuration provides for both overpressure protecti	on and redundancy. A single
10		regulator run in the Station is designed to handle the	existing load requirement of the
11		local distribution system.	
12			
13		The changes to the Middlebury Station from the Initi	al Proposal are primarily related to a
14		decrease in the footprint. The new location allowed	for a smaller footprint than the
15		location contained in the Initial Proposal.	
16			
17	Q11.	What is the height of the fence to be installed at each	Gate Station?
18	A11.	It is unchanged from the Initial Proposal. The fence	will be 6-foot high galvanized chain
19		link with one additional foot of barbed wire at the top	<u>)</u> .
20			
21	Q12.	Please describe the access and parking areas for each	Gate Station.

1	A12.	They are unchanged from the Initial Proposal. The access will consist of a 15-foot wide
2		stabilized pervious surface underlain by geogrid. The parking area will be large enough
3		for two vehicles and will consist of the same surface material as the access drive.
4		
5	Q13.	Please describe the Gate Station external lighting plans.
6	A13.	It is unchanged from the Initial Proposal Only limited night-time lighting will be needed
7		at each Gate Station, at the entrance and at the building. The lights will be 100-watt
8		floodlights or luminaries, angled downwards.
9		
10	Q14.	Please describe the valves and valve locations.
11	A14.	Other than the specific valve locations described below, the valve plans are unchanged.
12		Eight sectionalizing valves will be installed along the pipeline length to allow for
13		isolation of pipeline segments in the event that they need maintenance or in the case of an
14		incident. Valve spacing is dictated by the Code and is based on the class location of the
15		pipeline. The valve placement along the Transmission Mainline will exceed the
16		requirements of 49 C.F.R. Section 192.179 (Transmission Line Valves).
17		
18		A photograph of a VGS Mainline Valve ("MLV" or "Sectionalizing Valve") was
19		included as Exhibit Petitioner JH-6.2. A typical MLV site is shown in Exhibit Petitioner
20		Supp. JH-10 (2/28/13). Valve locations along the Transmission Mainline are identified in
21		Exhibit Petitioner JH-3 at the following mile points:
22		MLV 0 at the Colchester Tie-In, MP 0.0;

1		MLV 1 at Redmond Road, Williston, MP 7.56;
2		MLV 2 at Lincoln Road, Williston, MP 14.3;
3		MLV 3 at Charlotte Road, Hinesburg, MP 19.81;
4		MLV 4 at Hollow Road, Monkton, MP 26.48;
5		MLV 5 at Plank Road, New Haven, MP 32.4;
6		MLV 6 at Hunt Road, New Haven, MP 38.11; and
7		MLV 7 at Middlebury Gate Station, MP 41.24.
8		
9		3. <u>Project Construction</u>
10	Q15.	Please describe the pipeline construction process.
11	A15.	The process involves a series of sequential steps, as graphically illustrated on Exhibit JH-
12		13, previously provided. The pipeline construction process, which is essentially
13		unchanged from the December 20 Proposal, will generally proceed in the following
14		sequence:
15		1. The construction is expected to be sequenced from north to south although
16		there will be multiple construction sections called "spreads."
17		2. The route is first cleared and temporary work areas are prepared.
18		3. Perimeter erosion control measures, such as silt fences, are installed along
19		sensitive resource areas such as stream edges and wetlands to control
20		sediment.
21		4. For the Transmission Mainline, a four to five-foot wide trench will be
22		excavated to a depth of approximately five-feet, and soil from the trench will

1		be stockpiled adjacent to the trench within the construction corridor. There
2		will be different construction configurations for each of the different types of
3		area to be crossed, including wetlands, agricultural areas and within the public
4		highway ROW. These configurations are shown in Exhibit Petitioner Supp.
5		JH-3 (2/28/13). Smaller trenches of approximately four-feet by five-feet will
6		be used for the Distribution Mainlines.
7		5. Pipe lengths will be welded together, inspected, laid in the trench and warning
8		tape will be laid over the line, and then the trench will be backfilled. The pipe
9		will be covered by at least 36 inches of soil. The pipeline will have four-feet
10		of cover in agricultural areas, within the VELCO ROW and residential areas,
11		and generally five-feet of cover at road crossings and seven of feet cover at
12		open cut streams.
13		6. The landscape will be restored as close as possible to pre-construction
14		conditions in accordance with applicable permit requirements.
15		As Project Manager, it will be my responsibility to oversee that the Project is constructed
16		in accordance with all applicable Code and permit requirements.
17		
18	Q16.	Is water required for Project construction or operation?
19	A16.	The Project will not require the use of water for on-going operations. The three Gate
20		Stations are unmanned and therefore do not have sink or toilet facilities. However, as
21		part of construction, the Project will require approximately 1.4 million gallons of water to
22		hydrostatically pressure test the Transmission Mainline. The pipe will be hydrostatically

1		tested at a pressure of at least 2160 psi for a minimum of eight hours before being placed
2		in service. The test will prove there are no leaks and will validate the MAOP of 1440 psi.
3		For the hydrostatic test, water will be taken from a Town of Colchester municipal water
4		hydrant near the Colchester Tie-In. VGS has contacted the Champlain Water District
5		which supplies Colchester Fire District #3, where we propose to obtain the water for our
6		test. The Champlain Water District has stated that it will be able to provide the water
7		volume required. When the test is complete, the water will be discharged to a nearby
8		potential upland area at the tap as indicated on the Erosion Prevention and Sediment
9		Control Plans included with Mr. Nelson's prefiled testimony as Exhibit Petitioner Supp.
10		JAN-9 (2/28/13). These plans are being submitted as part as the Construction
11		Stormwater Discharge Permit to the Vermont Department of Environmental
12		Conservation, as discussed in more detail in Mr. Nelson's Supplemental testimony.
13		
14		The two sections of Distribution Mainlines will be tested independently with air at a
15		pressure of 190 psi for a period of eight hours.
16		
17		In addition, water, sourced from a local water hauler, will be used to control dust during
18		construction.
19		
20	Q17.	Has VGS identified the construction access points and laydown areas?
21	A17.	Yes. We have identified locations where access to the Transmission Mainline corridor
22		will be used as well as temporary work areas for equipment and materials staging areas.

1		These locations are identified in Exhibit Petitioner Supp. JH-3 (2/28/13) and were studied
2		by our environmental and cultural resource experts and are noted in the VHB natural
3		resources mapping, provided as an appendix to Exhibit Petitioner Supp. JAN-2 (2/28/13).
4		
5	Q18.	How will VGS manage construction waste?
6	A18.	Unchanged from the Initial Project, the generation of construction debris from the Project
7		will be minimal. Construction debris will be disposed of at an approved landfill. While
8		not generally considered construction waste, VGS will handle woody debris as follows:
9		trees under 6 inches in diameter, slash and brush will be chipped—not burned—and
10		spread along the ROW in upland areas. Trees greater than 6 inches in diameter will be
11		cut into logs, stacked in upland areas and offered to landowners along the ROW for
12		landowner use.
13		
14	Q19.	Will blasting be required for pipeline installation?
15	A19.	Yes, we anticipate that blasting will be required for approximately 35% of the proposed
16		route. The 2/28/13 Proposal requires similar levels of blasting to the Initial Proposal,
17		accordingly there is no change to the blasting protocols described below. Areas requiring
18		blasting will be further defined during the final design process. VGS will use a blasting
19		contractor licensed in the State of Vermont. It should be noted that blasting for projects
20		of this nature will have limited impacts. Any blasting that is required for the Project
21		would be conducted by state-licensed professionals in accordance with applicable
22		blasting codes and local blasting requirements. All blasting would be conducted during

1	daylight hours and would not begin until appropriate local authorities and the occupants
2	of nearby buildings, including residences and places of business, have been notified. In
3	general, blasting would involve installation of small drill holes, and the use of low energy
4	charges. Potential fracture impacts would be avoided through the use of open-face
5	blasting techniques, which would direct the energy of the blast upward to the surface
6	instead of downward. Delayed charges would be ignited in sequence to facilitate the
7	upward movement of rock along the rock face. VGS will also conduct pre-blast
8	inspections of nearby facilities and structures; install blasting mats to control the
9	scattering of loose rock; use warning signals, flags and barricades to limit access to the
10	blast area; and conduct post-blast surveys as necessary to assess damage.
11	Notwithstanding the limited impact of the blasting, VGS will adhere to a rigorous
12	blasting plan, highlights of which are described below.
13	
14	Pre-Blast Surveys/Notifications
15	Pre-blast surveys and Water Quality/Flow Testing will be offered to all property owners
16	that are within a 600-foot radius from the blast site. Appropriate notices will be given
17	and appointments arranged for those owners who desire a survey. Pre-blast surveys will
18	be conducted by a qualified firm approved by VGS. Results of those surveys will be
19	documented through video or still photographs and appropriate narration or written
20	reports.
21	

22 <u>Blast Monitoring</u>

1	All blasts will be monitored by a representative of a qualified firm approved by VGS who
2	has been properly trained in the setup and use of seismic monitoring equipment. At least
3	one seismograph will be in use at all times. Placement of monitoring equipment will be
4	at the nearest structure to the blast site. Results of blast monitoring will typically be
5	available before the next blast. Results can be reviewed and modifications can be made
6	to the blast design for the next blast if necessary.
7	
8	Sequence of Blasting
9	All blasting operations will be strictly coordinated with VGS's on-site representative and
10	local Fire Departments. Emphasis will be on the safe and efficient removal of the rock
11	existing on this project without impact to surrounding structures.
12	
13	Blasting Procedures
14	1. Blasting operations shall commence after 7:00 AM and cease before 7:00 PM,
15	Monday through Saturday.
16	2. Blasting cannot be conducted at times different from those announced in the
17	blasting schedule except in emergency situations, such as electrical storms or
18	public safety required unscheduled detonation.
19	3. Warning and all-clear signals of different character that are audible within a range
20	of one-quarter mile from the point of the blast shall be given. All persons within
21	the permit area shall be notified of the meaning of the signals through appropriate
22	instructions and signs posted.

1	4. Access to the blasting area shall be regulated to protect the public from the effects
2	of blasting. Access to the blasting area shall be controlled to prevent
3	unauthorized entry before each blast and until the perimeter's authorized
4	representative has determined that no unusual circumstances exist after the blast.
5	Access to and travel in or through the area can then safely resume.
6	5. Areas in which charged holes are awaiting firing shall be guarded, barricaded and
7	posted, or flagged against unauthorized entry.
8	6. Blasting mats shall be used to cover blasts and prevent fly rock.
9	
10	Blast Security
11	Each blast will be preceded by a security check of the affected area. Communications
12	will be made with job site supervisors and local officials as required to ensure the safest
13	possible operation. All personnel in the vicinity closest to the blast area will be warned.
14	
15	No blast will be fired until the area has been secured and determined safe. The blast site
16	will be examined by the blaster prior to the all-clear signal to determine that it is safe to
17	resume work.
18	
19	Blast Vibration
20	Blast vibration will be monitored at the blast site, typically at the structure(s) closest to
21	the blast site. Vibration limits will closely follow industry limits and the State and Local
22	Regulations. Blast designs will be modified as required to stay within the guidelines.

- Blasting operations will be modified accordingly when approaching buildings and
 utilities.
- 3
- 4

4. <u>Right of Way Acquisition</u>

5 Q20. Will the Project require ROW acquisition?

Yes. VGS will purchase easements from landowners along the Transmission Mainline 6 A20. 7 where public ROWs are not being used. Landowner parcels along the Final Alignment 8 are shown on Exhibit Petitioner Supp. JH-3 (2/28/13). VGS has contacted all landowners 9 along the pipeline route and is currently in discussions to obtain easements. As a result 10 of moving the alignment off of public roads in some locations at the request of the 11 communities, the 2/28/13 Alignment will require VGS to obtain easements associated 12 with approximately 200 land parcels. This is an increase of approximately 40 parcels 13 from the Initial Proposal. VGS is targeting to have all easements in place by the end of 14 2013.

- 15
- 16 5. <u>Noise Impacts</u>

17 Q21. Will the Project generate noise?

A21. During construction, the Project will generate general construction noise associated with
construction vehicles and equipment. Construction activities will normally occur
between 7 a.m. and 7 p.m. and will only last during the construction period. Once
constructed, because they are buried, the Project pipelines will not generate any
additional noise.

2		The sectionalizing valves are not pressure-reduction valves containing any mechanized
3		components, and therefore will not result in additional noise.
4		
5		VGS has selected a heater system for the Gate Stations that emits very little noise. VGS
6		has calculated that after construction of the Project and during the peak hour of operation,
7		the noise level at each Gate Station will be approximately 50 dBA when measured at the
8		fence line. The closest occupied structure (a bookstore in Middlebury) to any of our
9		proposed Gate Stations is approximately 150 feet. While this is closer than the nearest
10		occupied structure in the Initial Proposal, the Gate Station was relocated at the request of
11		the community, and at this distance, the noise is projected to drop well below the 45 dBA
12		nighttime and 55 dBA daytime noise levels required in other Board proceedings.
13		
14		6. <u>Transportation Impacts</u>
15	Q22.	What impacts will the Project construction have on traffic and transportation facilities?
16	A22.	We plan to conduct horizontal directional drilling ("HDD") or boring under a number of
17		street crossing and railway crossings, namely:
18		Mill Pond Road, Colchester; Uncased bore
19		Colchester Rd. (Route 2A), Essex; Uncased bore
20		New England Central RR, Essex; Cased bore
21		Upper Main St. (Route 15), Essex; Uncased bore
22		Essex Way, Essex; Uncased bore

1	River Rd. (Route 117), Essex; HDD with Winooski River
2	New England Central RR, Essex; Cased bore
3	Redmond Road at CSWD, Williston; Uncased bore
4	Mountain View Rd., Williston; Uncased bore
5	Williston Rd. (Route 2), Williston; HDD with Allen Brook
6	Interstate Highway 89, Williston; HDD
7	Hurricane Lane, Williston; Uncased bore
8	St. George Rd. (Route 2A), Williston; Uncased bore
9	St. George Rd (Route 2A), St. George; Uncased Bore
10	Vermont Route 116, St. George; Uncased bore
11	Shelburne Falls Road, Hinesburg; Uncased bore
12	Charlotte Road, Hinesburg; Uncased bore
13	Hollow Road, Monkton; Uncased bore
14	Monkton Road, Monkton; Uncased bore
15	Plank Road, New Haven; Uncased bore
16	North Road, New Haven; Uncased bore
17	Plank Road, New Haven; Uncased bore
18	Quarry Road, New Haven; Uncased bore
19	Main St. (Route 17), New Haven; Uncased bore
20	Town Hill Road, New Haven; Uncased bore
21	Hunt Road, New Haven; Uncased bore
22	River Road, New Haven; Uncased bore

1	Vermont Route 7, New Haven; Uncased Bore
2	Beldon Road, New Haven; Uncased Bore
3	HDD or boring involves the installation of pits at either side of the area to be crossed and
4	drilling or auguring the pipe beneath that area, creating no disturbance at the surface.
5	This technique, although more expensive, allows us to avoid direct impacts to these areas.
6	These locations reflect the route alignment changes previously described.
7	
8	In areas where we will install the pipe with traditional open-cut methods across
9	roadways, we will employ standard traffic control measures to maintain at least one lane
10	of traffic during installation. Additionally, there are areas where we will be installing
11	pipe within the road ROW or shoulder. In these areas we will employ traffic control
12	measures and maintain one lane of traffic during construction. Road surfaces will be
13	protected and restored to original or better condition if impacted by construction.
14	
15	During construction in these areas, VGS will utilize traffic control methods that comply
16	with Vermont Agency of Transportation ("VTrans") standards, including employment of
17	appropriate signage and the services of sheriffs or other traffic control personnel to
18	manage traffic flow. VGS will obtain highway permits from VTrans and local
19	municipalities for work in state and local roadways.
20	
21	The Winooski River is considered a navigable water under Section 10 of the Rivers and
22	Harbors Act of 1899, and is subject to the permit jurisdiction of the Army Corps of

1		Engineers ("ACOE"). As explained in Mr. Nelson's testimony, VGS has applied for a
2		Section 10 permit for this crossing. From a practical standpoint, this will have no impact
3		on river transportation and navigation, as we plan to HDD the crossing, and thus will not
4		impact surface waters.
5		
6		7. <u>Cost Estimate</u>
7	Q23.	Please provide the estimated cost of the Project.
8	A23.	The Project is estimated to cost \$86,612,944, which includes the proposed Transmission
9		Mainline and Distribution Mainlines; it does not include the distribution networks in
10		Middlebury and Vergennes. This reflects an increase of \$2.8 million, primarily
11		associated with additional HDD to mitigate environmental impacts as discussed in MR.
12		Nelson's supplemental testimony. A breakdown of the cost estimate is set forth in
13		Exhibit Petitioner Supp. JH-11 (2/28/13). The cost estimate was prepared using quotes
14		from equipment vendors, discussions with contractors familiar with the work and
15		historical costs from similar projects.
16		
17		8. <u>Schedule</u>
18 19	Q24.	What is the schedule for the Project?
20	A24.	The current schedule is to construct the Project in 2014. This will bring gas service to
21		anchor customers in the Middlebury industrial park by late 2014. The distribution
22		networks in Middlebury and Vergennes would be constructed in 2015, with residential
23		and commercial customers receiving gas service by the 2015/16 winter.

2 9. <u>Conclusion</u>

- 3 Q25. Does this conclude your testimony at this time?
- 4 A25. Yes, it does.